

ON THE KINETICS OF AlH_3 DECOMPOSITION AND THE SUBSEQUENT Al OXIDATION

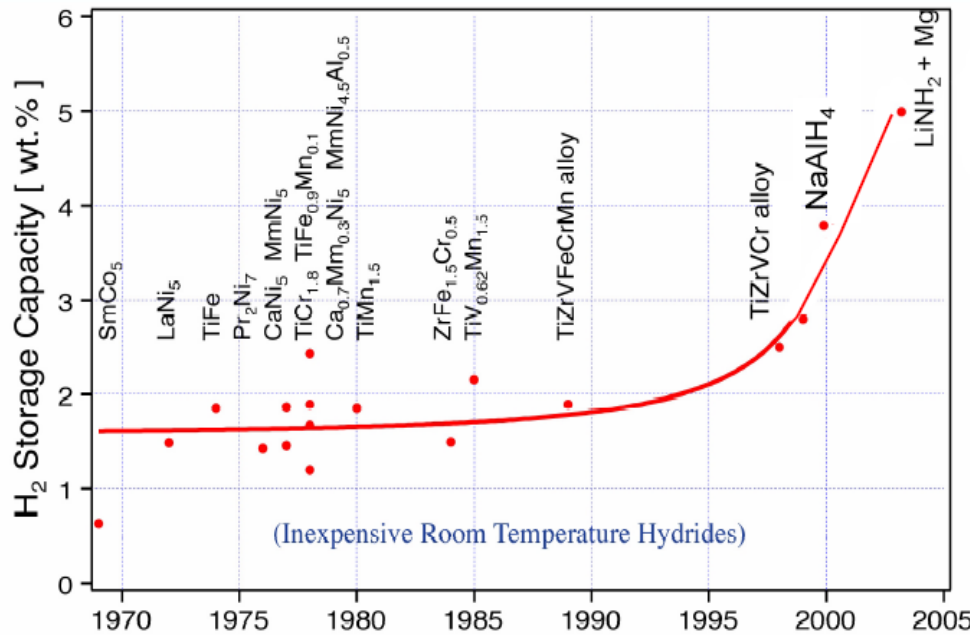
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Hydrogen storage:

- ⇒ High pressure tanks 350 – 700 bar or higher
in composites, mechanical stability
- ⇒ Liquid hydrogen tanks: boil-off, cooling/isolation,
safety
- ⇒ Solid hydrides
 - ⇒ Heavy metals: low gravimetric storage
 - ⇒ Light metals: adsorption in nano structures
 - ⇒ Light metals: chem.bonded hydrides

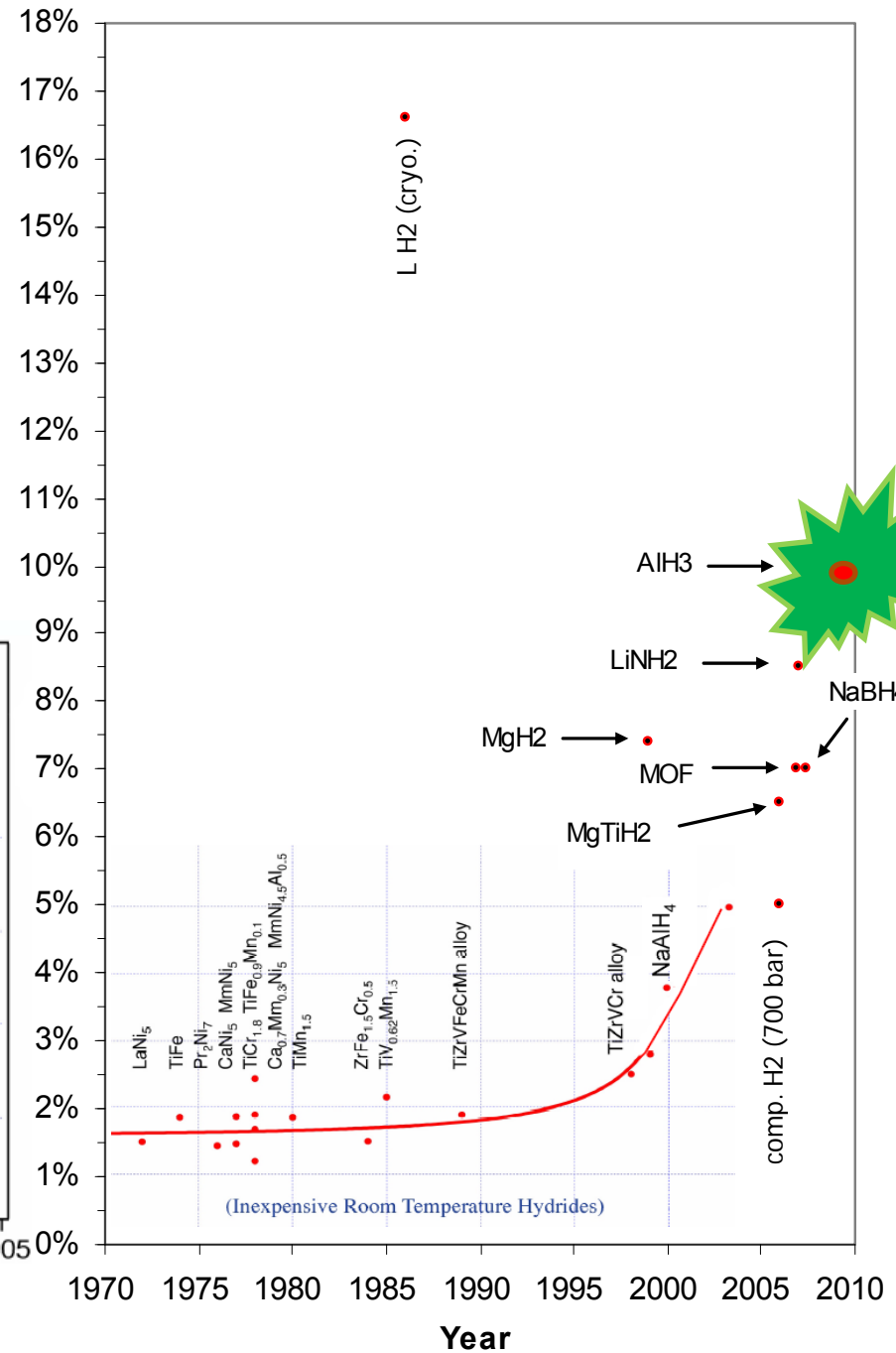
AlH₃ as model substance for storage of hydrogen hydride

Amorphous light metal powders are about 5%

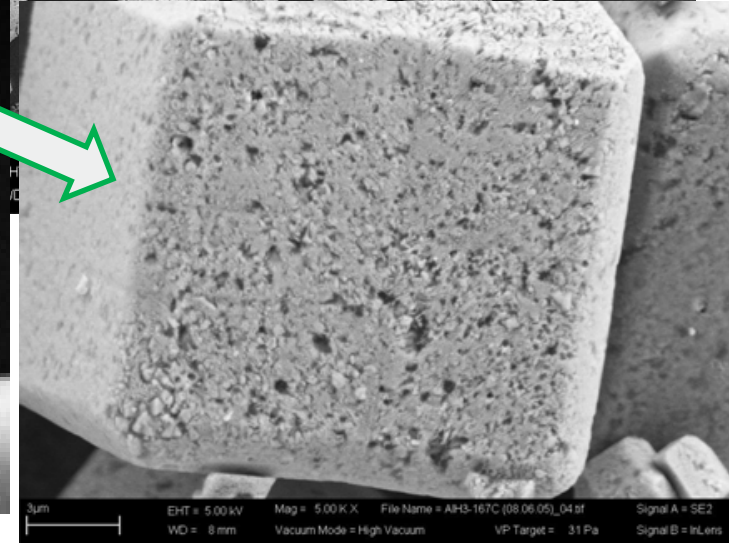
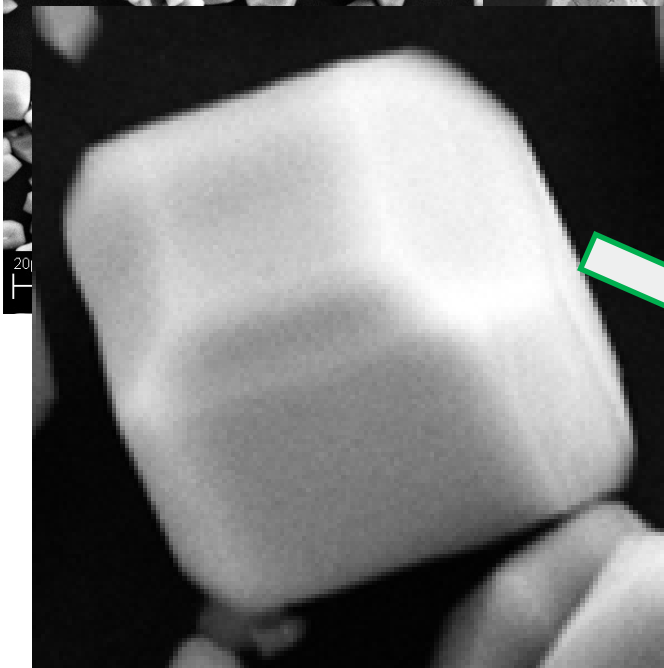
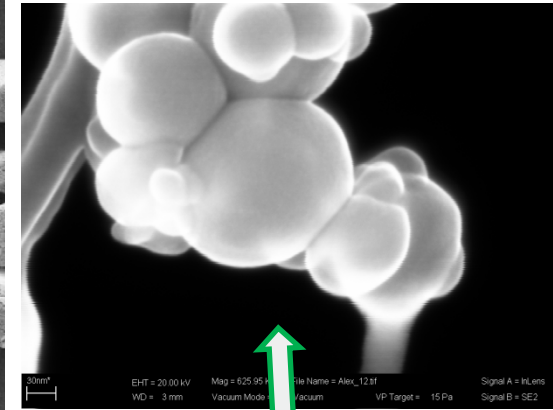
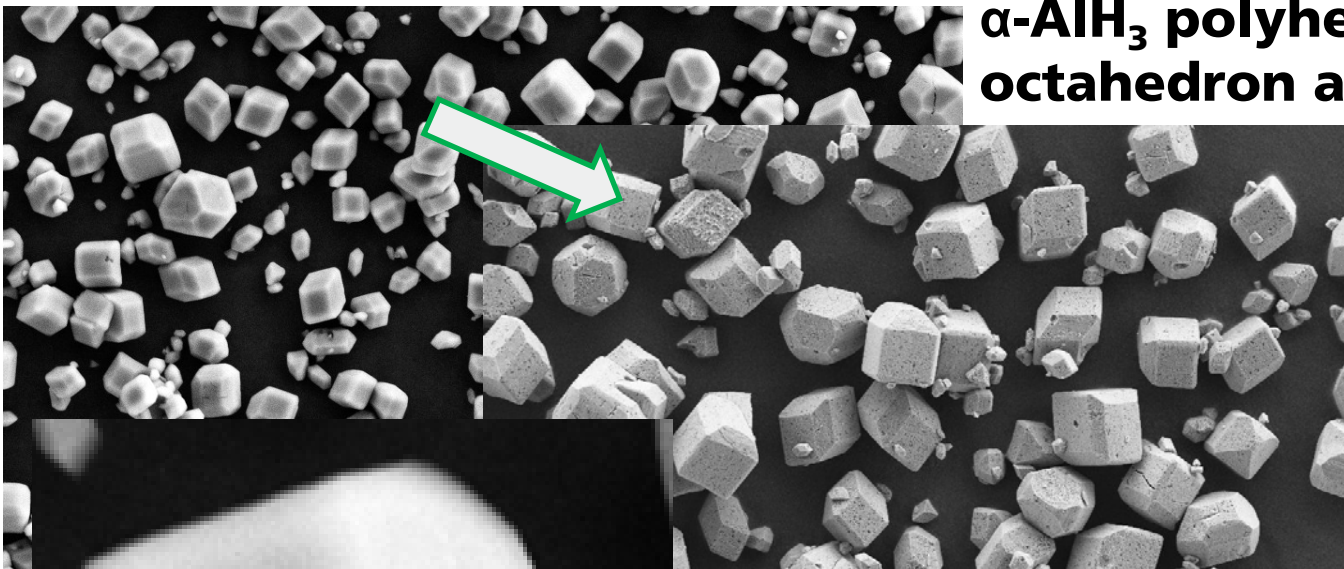


e Capacity (%)

Hydrogen Storage Systems - General Survey



α -AlH₃ polyhedra as cubes, cubic octahedron and hexagonal prisms



For comparison:
Alex: electro-exploded Al
surface **12.28 m²/g**

**Resulting Al is
not passivated
!!!**

On dehydrogenation => nano-porous Al structures emerge with
surface **15 to 20 m²/g** from AlH₃ of 0.69 m²/g surface area

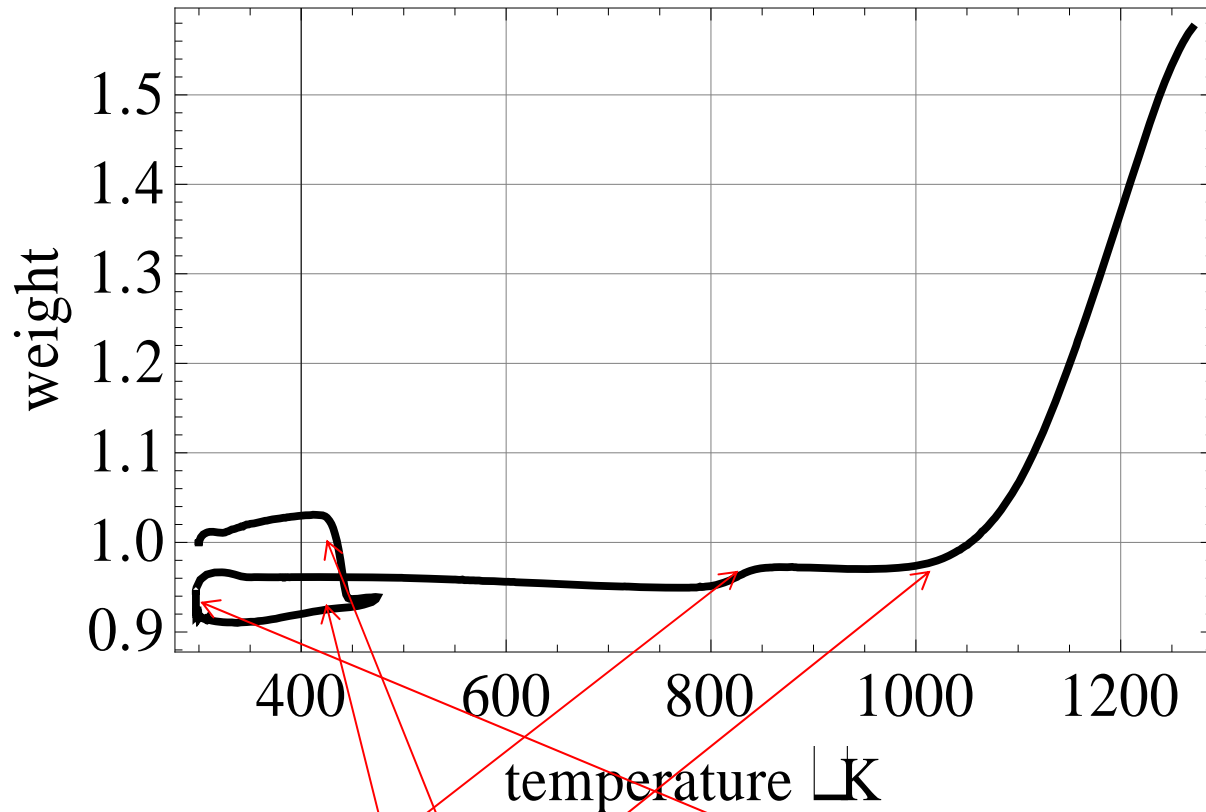
Risks arising from dehydrogenated hydrides*:

- The solids are highly porous or nano-structured to expose high surface areas to easy hydrogen access but also to easy air access on accidents.
- The metals => pure state, highly sensitive to oxidation if contact to air.
- The temperatures are elevated on operation in relation to oxidation reactions of metals, even they are considered moderate.
- In addition gaseous hydrogen is present

- Passivation reactions: thin protecting oxide layers (for Al ~ 2 – 4 nm)
=> 10-30% of metals might be oxidised at high reaction rates:
 - Thermal explosion of container and the subsequent distribution
 - Explosion of released metal of nano-size in air
 - Even a Deflagration Detonation Transfer might be possible if well distributed nano-particles in air ignite.

Investigation of this effect in more detail!!!

Al from dehydrogenated AlH_3 behaves like Al nano or ultra-fine particles



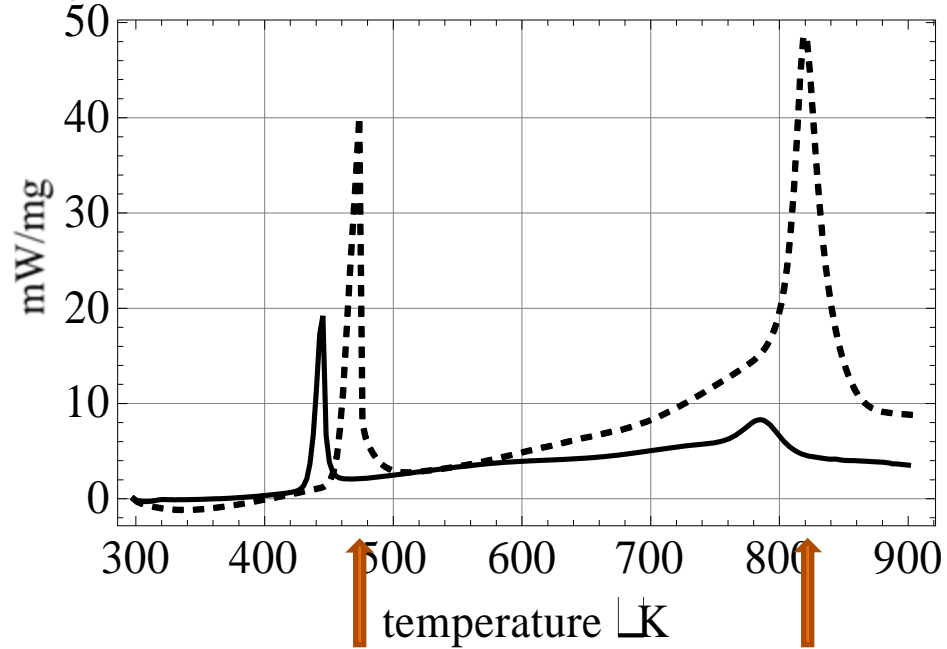
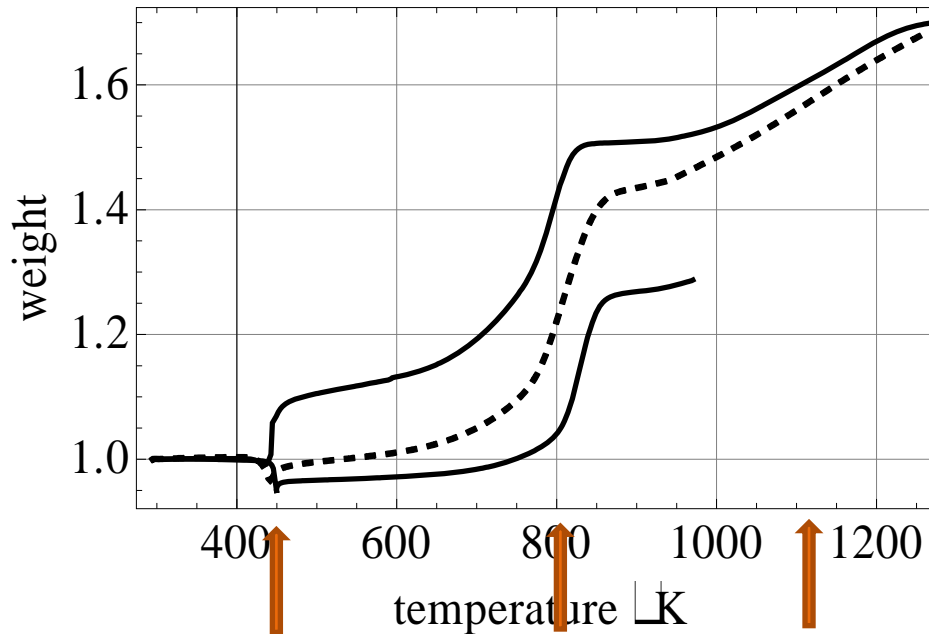
TG-curve heated (2 K/min) in an inert Ar-atmosphere till 480K initiating dehydrogenation, then cooled down to 50 K with air entrainment causing passivation and subsequent heating to 1300 K (5 K/min) with two steps of oxidation at 850 K and 1100 K

Modelling the reactions => kinetics for simulation of thermal explosions

TG in Air 2, 5, 10K/min

Methods of Thermal Analysis: DSC, TG, X-Ray

DSC in Air 2, 10 K/min



Dehydrogenation and formation of Al_2O_3 2-4nm passivation layer

chemical controlled 10 nm thick particle oxidation

diffusion controlled particle oxidation

Dehydrogenation and formation of Al_2O_3 2-4 nm passivation layer

Chemical Controlled 10 nm thick particle oxidation

**Reaction at 440 K: $AlH_3 \Rightarrow Al \Rightarrow Al\text{-crystallites} + O_2 \Rightarrow Al\text{-crystallites}$
with Alumina-layer (higher T, further oxidation)**

$$\frac{d[AlH_3]}{dT} = -n \frac{k_1(Z, E, T)}{A} [AlH_3] (-\ln[AlH_3])^{\frac{n-1}{n}} \quad \text{Alane dehydration = Avrami-Erofeev-Mechanism}$$

$$\frac{d[Al]}{dT} = \frac{d[AlH_3]}{dT} - \frac{k_{2,cryst}(Z, E, T)}{A} f_{cryst}([Al]) - \frac{k_{3,oxid}(Z, E, T)}{A} f([Al])$$

$$\frac{d[Al_2O_3]}{dT} = \frac{k_{3,oxid}(Z, E, T)}{A} f([Al]) \quad \text{Al passivation = 1st order oxidation-Mechanism}$$

Solution:

$$[Al] = ne^{-\frac{Z_2}{A} S_2(E_2, T)} \int_0^T k_1(u) \left(\frac{Z_1}{A} S_1(E_1, u) \right)^{n-1} e^{\frac{Z_2}{A} S(E_2, u) - \left(\frac{Z_1}{A} S_1(E_1, u) \right)^n} du$$

$$[Al]_{cryst} = \int_0^T k_2(u) [Al](u) du$$

$$[AlH_3] = e^{-\left(\frac{Z}{A} S(E, T) \right)^n}$$

$$[Al_2O_3] = \int_0^T k_4(u) [Al](u) du$$

$$k(Z, E, T) = Ze^{-\frac{E}{RT}}; S(E, T) = \int e^{-\frac{E}{RT}} dT = Te^{-\frac{E}{RT}} \sum_{n=1}^N n! (-1)^{n-1} \left(\frac{RT}{E} \right)^n$$

Kinetic model related to TG and DSC – curves

TG + DSC curves are constructed from the set of equations solving the reaction scheme by:

$$\text{TG}(T) = W_{\text{alane}} - W_{\text{hyd}} + p W_{\text{oxy}} ;$$
$$W_{\text{alane}} \sim [\text{AlH}_3], \quad W_{\text{oxy}} \sim [\text{Al}_2\text{O}_3], \quad W_{\text{hyd}} \sim [\text{Al}]$$

and the DSC curve by:

$$\text{DSC}(T) = Q_1 \frac{d[\text{AlH}_3]}{dT} + p Q_2 \frac{d[\text{Al}_2\text{O}_3]}{dT}$$

Least squares fit of TG(T) and DSC(T) to achieve E and Z the different reaction

Achieve kinetic parameters of alane dehydrogenation in a separate experiment with total exclusion of air

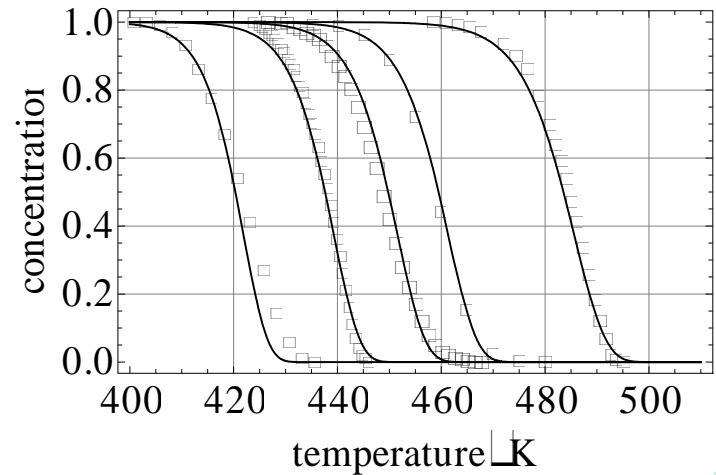
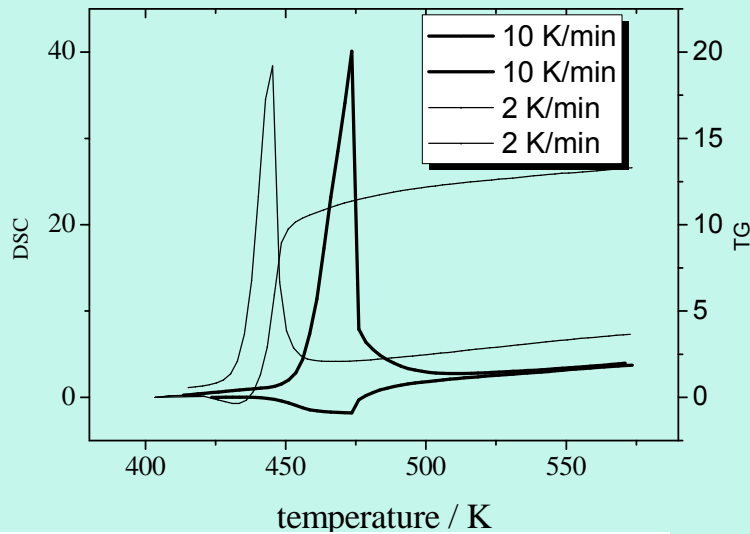
TG(T) = W = weight of TG curve

DSC(T) = DSC-curve

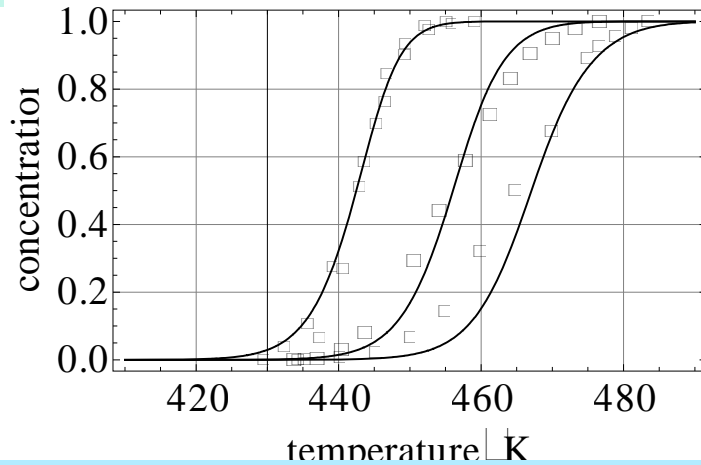
Q1 and Q2 = heat of reactions, p partial oxidation of Al in passivation reaction

Modelling of Alane dehydrogenation and passivation (at 450 K) – fit of TG / DSC curves at heating rates 0.5 -10 K/min

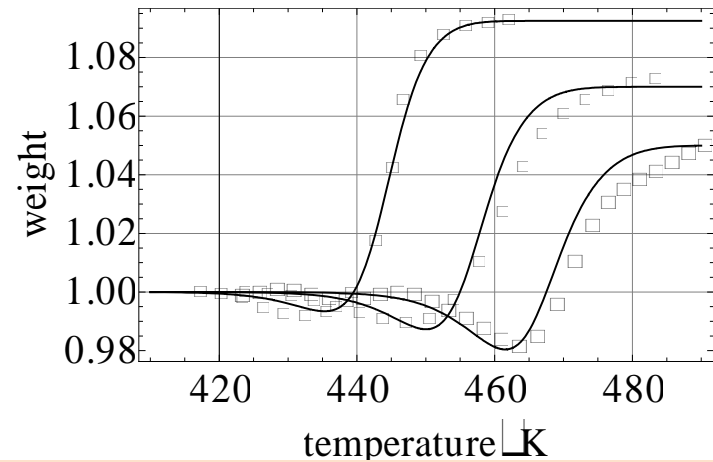
TG/DSC of dehydr. AlH_3 and Al passivation



TG of dehydrogenation AlH_3

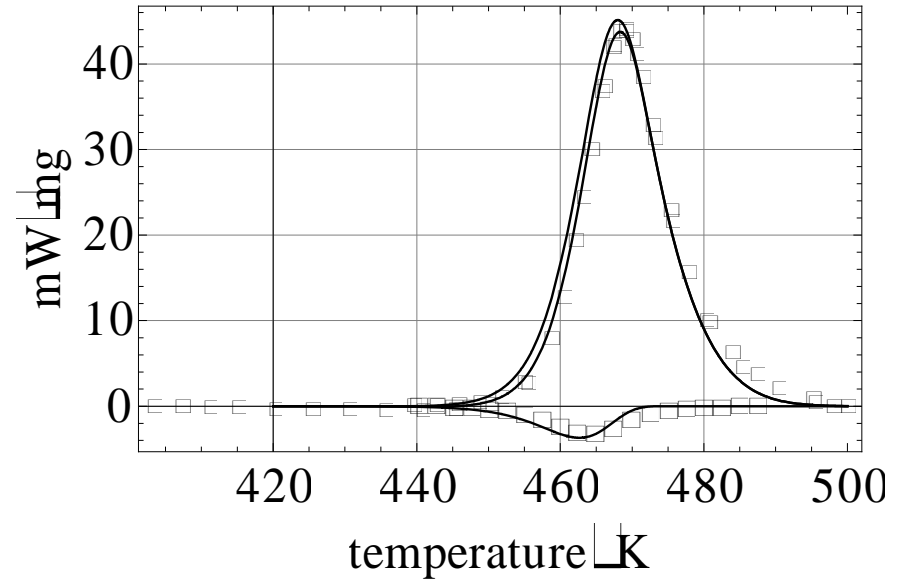
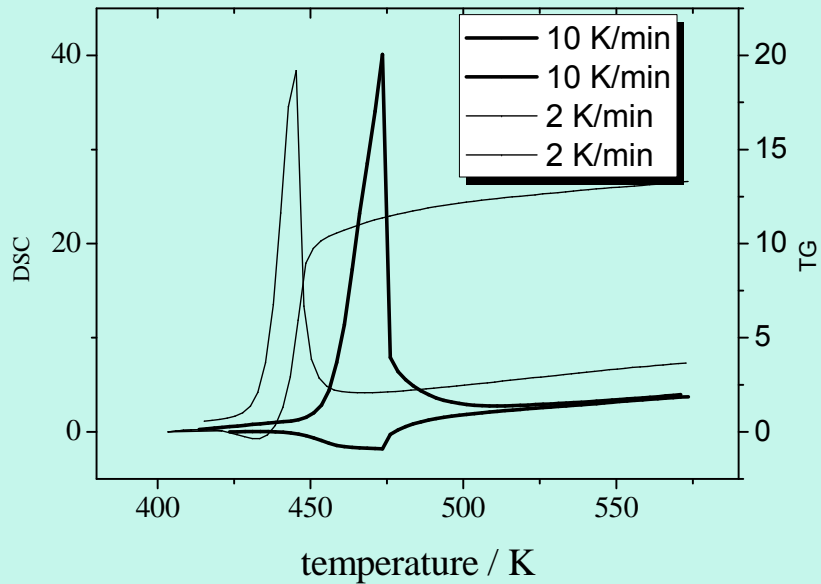


Recovered TG/conc. of dehydr. AlH_3

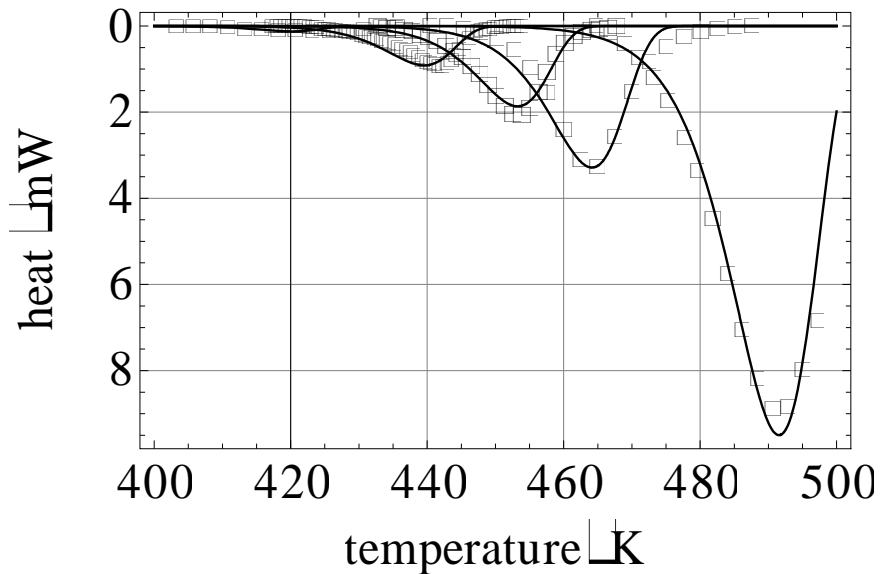


Fit of TG: dehydr. AlH_3 and Al passivation

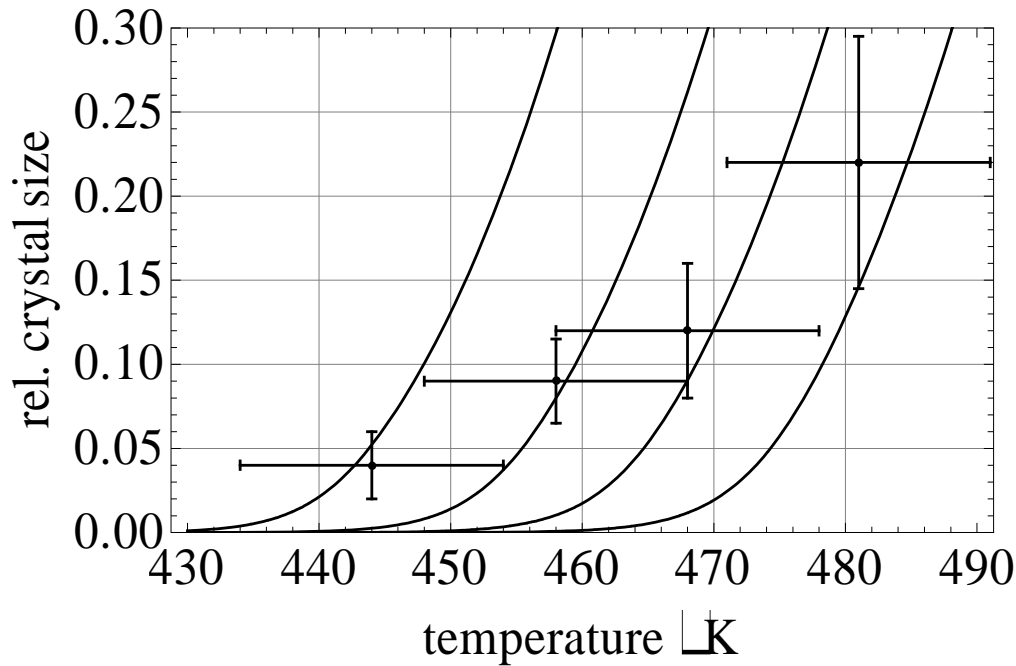
DSC-curve of dehydrogenation in Argon subtracted from DSC-curve in air



Fit of DSC: dehydrogenation of AlH₃ and Al passivation at 10K/min



DSC fit of dehydrogenation AlH₃ at 4 heating rates



Crystal growths estimated from weight increase on passivation depending on the heating rate 2, 5, 10 and 20 K/min

At higher temperatures of dehydrogenation, less surface area is available for passivation and therefore for the oxidation reaction, which might lead to hazardous thermal explosion

Results of kinetic parameters / discussion of kinetic compensations effect in the paper

Method: evaluated simultaneously	Dehydrogenation TG-DSC	Dehydrogenation TG-DSC (fitted n)	Oxidation TG- DSC
Activation energy [J]	115031	117770	83077
Pre-expon. Log Z	11.04	11.37	7.62
Avrami-Erofeev order n	3	2.58	3